

# The Processivity of Kinesin-2 Motors Suggests Diminished Front-Head Gating

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## Summary

Kinesin-2 motors, which are involved in intraflagellar transport and cargo transport along cytoplasmic microtubules, differ from motors in the canonical kinesin-1 family by having a heterodimeric rather than homodimeric structure and possessing a three amino acid insertion in their neck linker domain. To determine how these structural features alter the chemomechanical coupling in kinesin-2, we used single-molecule bead experiments to measure the processivity and velocity of mouse kinesin-2 heterodimer (KIF3A/B) and the engineered homodimers KIF3A/A and KIF3B/B and compared their behavior to *Drosophila* kinesin-1 heavy chain (KHC). Single-motor run lengths of kinesin-2 were 4-fold shorter than those of kinesin-1. Extending the kinesin-1 neck linker by three amino acids led to a similar reduction in processivity. Furthermore, kinesin-2 processivity varied inversely with ATP concentration. Stochastic simulations of the kinesin-1 and kinesin-2 hydrolysis cycles suggest that “front-head gating,” in which rearward tension prevents ATP binding to the front head when both heads are bound to the microtubule, is diminished in kinesin-2. Because the mechanical tension that underlies front-head gating must be transmitted through the neck linker domains, we propose that the diminished coordination in kinesin-2 is a result of its longer and, hence, more compliant neck linker element.

## Results and Discussion

Kinesin processivity relies on maintaining the hydrolysis cycles of the two heads out of phase such that one head remains bound to the microtubule at all times. Figure 1A shows our working model for the kinesin-1 hydrolysis cycle that accounts for a large body of kinesin mechanical and biochemical experiments [1]. Features of the hand-over-hand model that ensure processivity can be described by two nonexclusive mechanisms: front-head gating and rear-head gating (for consistency with the literature, we use the term “gating” but emphasize that this refers to gating of a given head and not gating by a given head) [2–5]. Both of these mechanisms involve mechanical tension between the two heads that is transmitted through the flexible neck linker of each head and their shared neck coiled-coil domain. In front-head gating, rearward strain on the leading head in state 1 prevents ATP

from binding until the trailing head detaches (state 2). This mechanism prevents premature ATP hydrolysis and subsequent detachment of the leading head and ensures that the trailing head is primed to advance to the next binding site when ATP binds to the leading head. In the rear-head gating model, the bound head in state 4 dissociates slowly in comparison to the overall cycle time, and binding of the second head (state 1) produces forward strain that leads to rapid detachment (state 2).

Because both front-head gating and rear-head gating involve mechanical tension between the head domains, modifications that increase the mechanical compliance of the flexible neck linker are predicted to reduce motor processivity. Based on sequence alignments and comparisons of crystal structures, the neck linker domain in kinesin-2 motors is three amino acids longer than the neck linker domain of kinesin-1 (17 versus 14 amino acids) (Figure 1B). If this extension increases the compliance of the neck linker, then either front-head gating, rear-head gating, or both mechanisms may be diminished in kinesin-2. This prediction was tested by measuring the processivity of kinesin-1 and kinesin-2 motors and interpreting the results with a stochastic model of the hydrolysis cycle.

## Kinesin-2 Is Less Processive Than Kinesin-1

The velocities and run lengths of individual KIF3 and KHC motors attached to polystyrene beads were analyzed first at saturating ATP levels. Motor dilution profiles were generated to ensure that experiments were carried out in the single-molecule regime (see Supplemental Data available online). The mean velocity of the KIF3A/B heterodimer was  $436 \pm 129$  nm/s (mean  $\pm$  SD,  $n = 90$ ), and the velocity of KHC motors was  $703 \pm 136$  nm/s ( $n = 58$ ). The KIF3 homodimers KIF3A/A ( $455 \pm 115$  nm/s,  $n = 101$ ) and KIF3B/B ( $458 \pm 106$  nm/s,  $n = 102$ ) had similar velocities to the wild-type heterodimer. Whereas the KIF3B/B velocity was consistent with previous measurements from gliding assays, the KIF3A/B and KIF3A/A velocities were significantly higher than previously reported [6]. The velocity differences are due to mutations that were discovered in the motors used in the previous work (see Supplemental Data); all of the velocities presented here are from the corrected sequences.

In contrast to velocity differences, which were within a factor of two, the run length of wild-type kinesin-2 was  $\sim 4$ -fold shorter than that of kinesin-1. The mean run length for KIF3A/B was  $449 \pm 30$  nm (mean  $\pm$  SEM,  $n = 88$ ) compared to  $1747 \pm 199$  nm ( $n = 57$ ) for KHC (Figure 2). The reduced processivity of kinesin-2 is consistent with the hypothesis that the longer neck linker domain in kinesin-2 reduces the degree of mechanical communication between the two heads and “uncouples” the hydrolysis cycles of the two heads. To test this hypothesis more directly, we extended the 14 amino acid neck linker of kinesin-1 by inserting the last three amino acids of the kinesin-2 neck linker (DAL) into kinesin-1 at the neck linker/neck coil junction. The run length of this kinesin-1<sub>+DAL</sub> construct ( $355 \pm 14$  nm) was 5-fold shorter than that of wild-type (Figure 2), consistent with disruption of the mechanochemical coupling between the two heads. Despite the significant reduction in processivity, kinesin-1<sub>+DAL</sub> moved at  $552 \pm 103$  nm/s,

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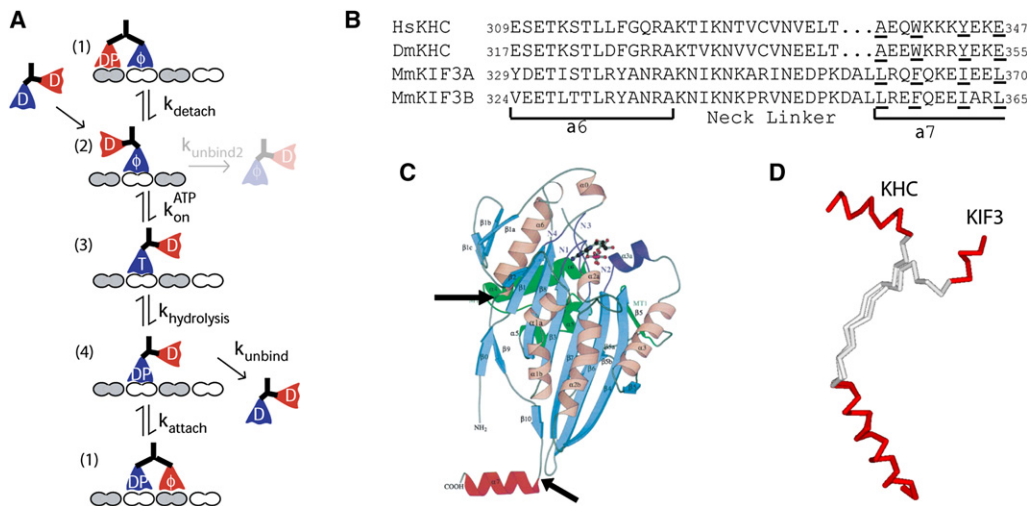


Figure 1. Kinesin Model and Structural Comparison

(A) Working model for the kinesin-1 chemomechanical pathway. T, ATP; D, ADP; DP, ADP.P<sub>i</sub>;  $\phi$ , no nucleotide. Motors in solution have high affinity for ADP and, upon binding to the microtubule (state 2), release one ADP molecule [20]. The motor waits in this state until ATP binds to the front head, which results in the docking of the neck linker and a displacement of the tethered head toward the next binding site (state 3) [21]. While the tethered head diffusively searches for the next binding site, the ATP on the bound head is hydrolyzed (state 4). Following hydrolysis (state 4), there are two possibilities. Most of the time (~99% for kinesin-1), the tethered head will bind to the next binding site and release its ADP (state 1), and then the rear head will detach (state 2), completing an 8 nm step. Alternatively, the bound ADP.P<sub>i</sub> head in state 4 will unbind from the microtubule, terminating the processive run. Whereas detachment from state 4 is the predominant termination step, at limiting ATP concentrations, the motor can occasionally detach from state 2.

(B) Neck linker sequences for kinesin-1 and kinesin-2 motors. The sequences of human conventional kinesin heavy chain (HsKHC), *Drosophila melanogaster* kinesin (DmKHC), and mouse KIF3A and KIF3B were aligned based on the known crystal structures of KHC (PDB: 3KIN, 2KIN, and 1MKJ) and KIF3 (3B6U). The kinesin-1 neck linker is defined as the 14 amino acids that span between the end of  $\alpha_6$  and the first hydrophobic residue of the  $\alpha_7$  coiled coil (A<sub>323</sub> to T<sub>336</sub> in human numbering). The start of the  $\alpha_7$  coiled coil was taken from the rat kinesin-1 dimer structure (3KIN) and the human KIF3B (3B6U) and *Giardia* KIF3A (GiKIN2a) monomer structures [22]. Hydrophobic a and d residues in the heptad repeat are underlined.

(C) Crystal structure of rat monomeric conventional kinesin from [23], showing the start and end of the 14 residue neck linker in kinesin-1.

(D) Comparison of the length and conformation of the KHC and KIF3B neck linkers. The figure was created by aligning the  $\alpha_6$  helix of the 2KIN and 3B6U structures.

only 20% slower than wild-type kinesin-1. The behavior of kinesin-1<sub>+DAL</sub> is qualitatively consistent with work from Hackney, who found that the biochemical processivity of *Drosophila* kinesin-1 was reduced when the neck linker was artificially extended [7]. However, it contrasts with recent results from Yildiz et al., who extended the neck linker of Cys-lite human kinesin-1 and found that the processivity fell by less than a factor of two for inserts as large as 29 amino acids [8]. Possible explanations for why the Yildiz results differ from ours include: (1) their use of a cys-lite modified kinesin, which

has been shown to have altered motor kinetics [4], (2) the use of axonemes rather than taxol-stabilized microtubules, (3) the inclusion of two positively charged lysines in the inserts, and (4) the low ionic strength buffer (12 mM PIPES versus 80 mM PIPES used here), which will enhance electrostatic tethering of the motors to the axonemes.

The measured run lengths of KIF3A/A and KIF3B/B were in the range of KIF3A/B, but the KIF3A/A run length ( $410 \pm 35$  nm,  $n = 85$ ) was moderately shorter than KIF3A/B, whereas the KIF3B/B run length ( $704 \pm 81$ ,  $n = 83$ ) was somewhat longer

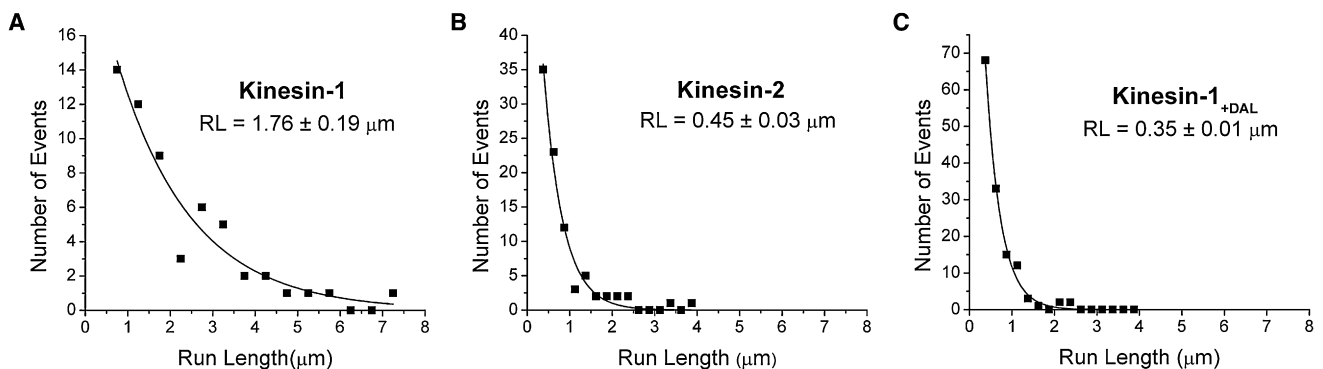


Figure 2. Run Length Distributions for Single Kinesin-1, Kinesin-2, and Kinesin-1<sub>+DAL</sub> Motors Attached to Beads

(A–C) Run lengths were estimated by fitting the data to an exponential in which the first bin (0–0.5  $\mu\text{m}$  for kinesin-1 and 0–0.25  $\mu\text{m}$  for kinesin-2 and kinesin-1<sub>+DAL</sub>) was ignored due to uncertainties in detecting events below 250 nm. Error bars represent SE of fits.

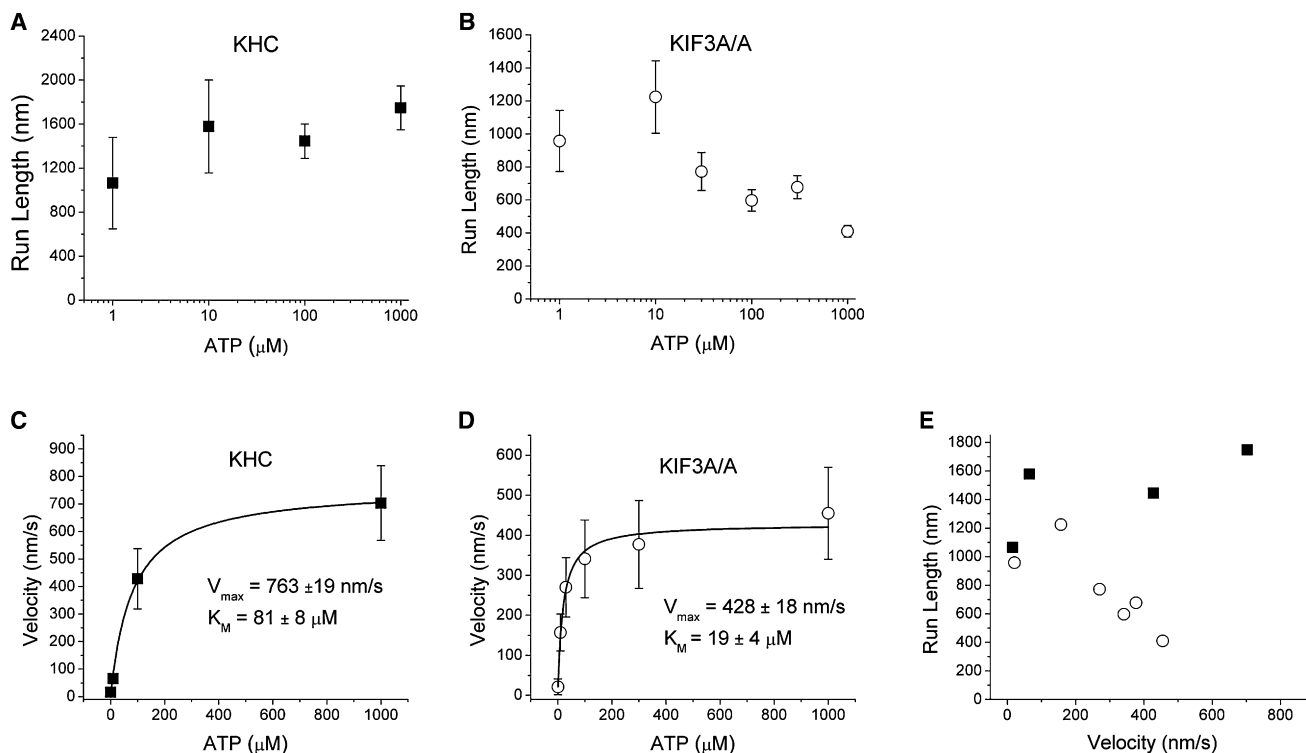


Figure 3. ATP Dependence of Motor Velocity and Run Length for KHC and KIF3A/A

(A–D) Run lengths (A and B) were obtained by fitting exponentials to the run length distribution at each ATP concentration; errors are SE of fits. Velocity data (C and D) are plotted as mean  $\pm$  SD for each concentration along with a fit to the Michaelis-Menten equation. The total number of events for KHC was 290 and for KIF3A/A was 467.

(E) Data are plotted as run length versus velocity to emphasize the different trends for KHC (solid squares) and KIF3A/A (open circles).

(see Supplemental Data for further details). Hence, although the heterodimeric structure of KIF3A/B is highly conserved between diverse species, the ability of the motor to take multiple steps before detaching does not require the presence of two different motor domains.

#### KIF3A/A Run Length Is ATP Dependent

We next measured the ATP dependence of the motor run lengths and velocities from 1  $\mu\text{M}$  to 1 mM ATP. We measured a weak positive dependence of kinesin-1 processivity on ATP, with slightly longer run lengths observed at higher ATP concentrations (Figure 3A). However, differences between the run lengths at 1  $\mu\text{M}$  and 1 mM ATP were not statistically significant ( $p = 0.07$  from paired  $t$  test), and these data are essentially consistent with Yajima et al., who found the processivity of kinesin-1 to be independent of ATP [9].

Whereas low ATP concentrations had no effect on the relative activity of kinesin-1, at ATP concentrations of 10  $\mu\text{M}$  and below, no binding events were observed for KIF3A/B in bead assays, and no microtubule landing was observed in microtubule gliding assays (data not shown). Nucleotide-free kinesin-1 is known to denature or misfold over time [10], and we interpret the KIF3A/B inactivation as an analogous process that has a greater nucleotide sensitivity. Interestingly, whereas KIF3B/B displayed similar inactivation at low ATP levels, KIF3A/A retained its function down to 1  $\mu\text{M}$  ATP, suggesting that it is the KIF3B head that inactivates in low nucleotide environments. Therefore, to investigate the ATP dependence of motor velocity and processivity, the behavior of KHC and KIF3A/A were compared.

In contrast to KHC, KIF3A/A run lengths fell from roughly 1 micron at low ATP concentrations to  $\sim 400$  nm at 1 mM ATP (Figure 3B). A paired  $t$  test showed statistically significant differences when comparing the run length at 1 mM to run lengths at 1  $\mu\text{M}$  and 10  $\mu\text{M}$  ATP ( $p = 0.02$  and  $p = 0.002$ , respectively). To exclude the possibility that multimotor interactions occur preferentially at low ATP, the KIF3A/A motor/bead ratio was decreased by a factor of two at 1  $\mu\text{M}$  ATP; no change in the run length was observed (run length  $1260 \pm 160$  nm [mean  $\pm$  SEM,  $n = 20$ ]). To normalize for the different  $K_M^{\text{ATP}}$  values and better show the run length differences, we plotted the data in Figure 3E as run length versus velocity, showing the clear processivity differences between KHC and KIF3A/A.

#### Kinetic Model Simulations

To better understand the chemomechanical cycle of kinesin-2 and to interpret processivity and velocity differences between kinesin-1 and kinesin-2 motors, we developed a stochastic computational model of the kinesin chemomechanical cycle. Existing kinetic models that use sets of linked ordinary differential equations are valuable for interpreting enzyme kinetic data [11], but these models are suboptimal for modeling processivity, and they are unable to model heterodimers with heads possessing different kinetics. Instead, we developed a Monte Carlo model that contains discrete states corresponding to different nucleotide states in the kinesin hydrolysis cycle and uses the Gillespie algorithm [12] to convert rate constants to expected transition times between states. To compare to the experimental data, we modeled many “runs” and calculated the mean velocity and run length. Initial rate constants for the

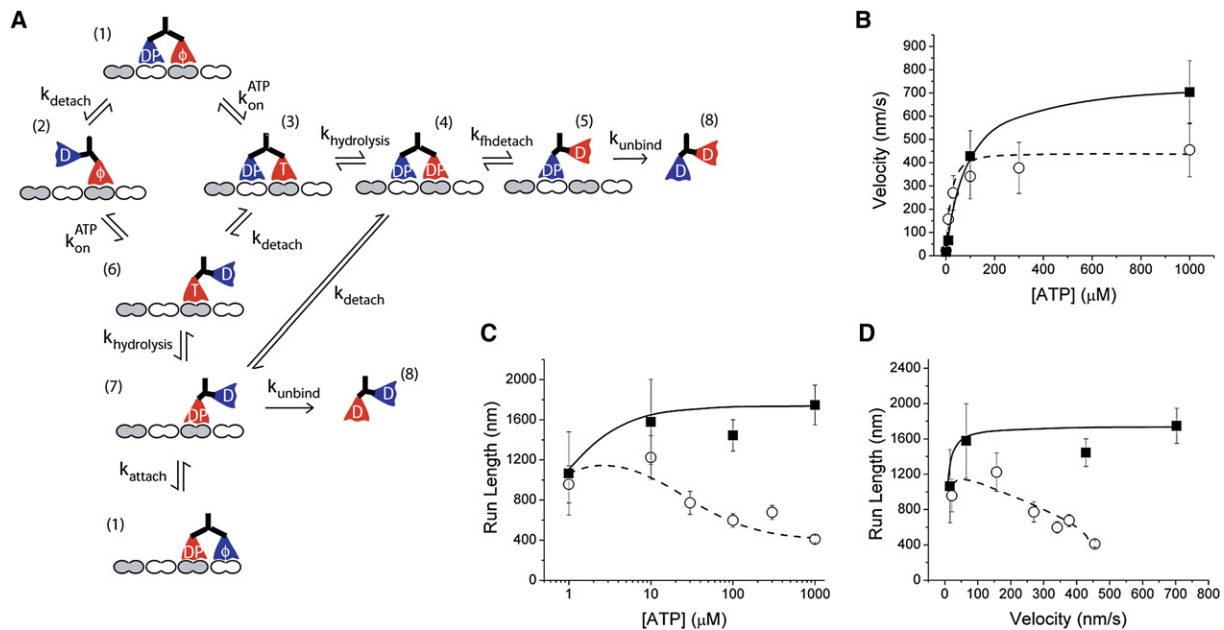


Figure 4. Kinesin-2 Model and Simulations

(A) Proposed model for the kinesin-2 chemomechanical pathway. Due to the enhanced compliance between the heads, ATP binding to the leading head in state 1 is allowed, leading to a bifurcation in the pathway that dominates at saturating ATP. As in the kinesin-1 model, slow detachment from state 2 waiting state is allowed but, for clarity, is not shown.

(B) Experimental results (symbols) and model simulations (lines) of motor velocity versus ATP concentration for KHC (solid squares and solid line) and KIF3A/A (open circles and dashed line). Model parameters are given in the Supplemental Data.

(C) Run length versus ATP concentration.

(D) Results at different ATP concentrations are replotted as run length versus velocity to emphasize the qualitatively different behavior of KHC and KIF3A/A.

kinesin-1 pathway (Figure 1) were taken from the literature, and selected rate constants were then systematically varied to match the experimentally observed velocity, run length, and  $K_M^{\text{ATP}}$  of KHC. As seen in Figure 4, the model is able to reproduce the ATP dependence of run length and velocity for KHC. Final model parameters and details of the simulations are described in the Supplemental Data.

We next investigated whether this model is sufficient to account for the KIF3A/A results. By adjusting specific rate constants, the reduced KIF3A/A run length and ATP dependence of velocity could easily be accounted for, but the model was unable to reproduce the ATP dependence of the run length. Inspection of the model in Figure 1 makes this clear—limiting ATP slows the kinetic cycle by extending the wait in the nucleotide-free state 2, which either has no effect or increases the probability of detachment at low ATP. Hence, to account for the observed behavior of KIF3A/A, the kinetic model has to be expanded to include other mechanochemical states.

As discussed in the Introduction, kinesin-1 processivity can be explained either by gating of the front head (tension-induced inhibition of ATP binding) or gating of the rear head (detachment triggered by attachment of the front head) [1–5]. Whereas the shorter run lengths for kinesin-2 could be accounted for in the model by diminishing the degree of rear-head gating (i.e., increasing  $k_{\text{unbind}}$  and/or decreasing  $k_{\text{attach}}$ ), those modifications did not reproduce the observed ATP dependence of processivity (data not shown). As a second approach, the front-head gating mechanism was disrupted by allowing ATP binding by the leading head to precede detachment of the trailing head (Figure 4A). If ATP binds to the leading head and is hydrolyzed before the trailing head

detaches, this puts both heads in a lower affinity state, which can lead to the motor detaching from the microtubule. This diminished front-head gating has a negligible effect at low ATP concentrations because the trailing head is able to detach before ATP binds (state 2), and the kinetic cycle collapses to the standard cycle shown in Figure 1. In contrast, at saturating ATP concentrations, ATP binds to the front head before the trailing head has time to detach (state 3), leading to possible premature termination of the cycle and shorter run lengths.

Initial rate constants for the KIF3A/A kinetic cycle were taken from the KHC simulations, and  $k_{\text{on}}(\text{ATP})$ ,  $k'_{\text{on}}(\text{ATP})$ ,  $k_{\text{hydrolysis}}$ , and  $k_{\text{unbind}}$  were iteratively adjusted to fit the measured KIF3A/A velocity, run length, and  $K_M^{\text{ATP}}$ . The fits of the expanded model to the experimental KIF3A/A velocity and run data are shown in Figure 4. Hence, relaxing the requirement that ATP binding to the leading head precedes detachment of the trailing head introduces a second detachment pathway that can account for the measured ATP dependence of KIF3A/A processivity. Below, we argue that the longer neck linker of kinesin-2 is sufficient to explain this partial uncoupling of the kinesin-2 mechanochemical cycle.

#### Mechanical Properties of the Neck Linker Domain

Disordered regions of proteins can be modeled as entropic springs, and the worm-like chain (WLC) model is commonly used to describe their force extension characteristics [8, 13, 14]. Modeling the neck linker as a WLC, the force necessary to extend the polymer a distance of  $x$  is:

$$F = \frac{k_B T}{l_p} \left[ 4 \left( 1 - \frac{x}{L} \right)^{-2} + \frac{x}{L} - \frac{1}{4} \right]$$

wherein  $k_B T$  is Boltzmann's constant times the absolute temperature (4.1 pN-nm);  $l_p$  is the persistence length of the polymer, estimated to be 0.5 nm [13–15]; and  $L$  is the contour length of the polymer, which we take as 0.38 nm per amino acid [16]. If (1) both heads of the motor are bound to a microtubule, (2) the two core motor domains take on identical conformations such that the neck linkers originate from  $\alpha_6$  at the same relative position, and (3) the neck coil does not unfold, then each flexible neck linker must extend to 4.1 nm to span the 8.2 nm tubulin repeat distance. From the above WLC model, the resulting tension on a 14 residue neck linker would be 43 pN, and the tension on a 17 residue neck linker would be 18 pN; both of these values are significantly greater than the  $\sim 6$  pN stall force of kinesin-1. Although these forces can be adjusted down somewhat by assuming different WLC model parameters or allowing elastic deformation of the heads or partial unfolding of the coiled-coil domain (see Supplemental Data), the important result here is that extending the neck linker is expected to significantly reduce the tension between the head domains when both heads are bound to a microtubule (state 1).

Because both front-head and rear-head gating rely on mechanical tension transmitted through the neck linker domain, the extended neck linker in kinesin-2 is expected to diminish both of these mechanisms. Gating of the rear head will be reduced because the tension that accelerates rear-head detachment will be diminished, whereas gating of the front head will be reduced because the tension that blocks ATP binding will be diminished. Because the predicted forces differ significantly (43 pN versus 18 pN), extending the neck linker could significantly alter the rate constants governing these transitions. For instance, if the characteristic distance associated with rear-head detachment is 0.5 nm, then from the Bell model  $k_{off}(F) = k_{off}^0 e^{-\frac{F x_{off}}{k_B T}}$ , the load-induced detachment rate will be 20-fold slower in kinesin-2 [17, 18]. Hence, it is reasonable to expect that the extended neck linker in kinesin-2 motors will result in significant differences in mechanochemical coupling between the two motor domains compared to kinesin-1.

### Implications for In Vivo Motor Behavior

What are the implications of this work for the function of kinesin-2 motors in vivo? Whereas the role of kinesin-1 is to transport cargo along axons that can be centimeters in length, kinesin-2 primarily transports cargo along flagella and cilia, which are only tens of microns. However, both of these transport distances are much longer than the single-molecule run lengths, and in cells, motor accumulations that enhance processivity as well as competition from cargo-associated dyneins that reverse the direction of transport will play important roles. This single-molecule characterization of kinesin-2 serves as an important foundation for future cell biological experiments aimed to understand the roles of kinesin-2 motors in cells.

### Experimental Procedures

#### Protein Purification and Bead Assay

Full-length His-tagged *Drosophila melanogaster* kinesin heavy chain and kinesin-1<sub>DAL</sub> were bacterially expressed, and KIF3 motors were baculovirus expressed and purified as previously described [2, 6]. Mutations discovered in the KIF3 plasmids used previously [6] were corrected with QuikChange Multi Site-Directed Mutagenesis (Stratagene, Inc.) (see Supplemental Data).

For bead assays, motors were adsorbed to 560 nm diameter, casein-passivated carboxylated polystyrene beads as previously described [19]. A weak optical trap was used to facilitate motor-microtubule interactions. Motor:bead ratios were chosen such that  $\leq 20\%$  of the beads moved

when brought in contact with microtubules. Bead positions were tracked manually with Meta-View. Run length data were fit with Origin 7.0. Details on the bead assays, optical trap, and motor dilution profiles are provided in the Supplemental Data.

### Model Simulations

Stochastic models were implemented in MATLAB. Transition times between states were determined with the Gillespie algorithm,  $t = \frac{1}{k} \ln \frac{1}{\text{rand}\#}$ , in which  $k$  is the first-order rate constant and rand# is a random number between 0 and 1 [12]. Runs were terminated when the motor detached, and the mean velocity and run length were calculated from 10,000 simulated runs for each condition. Further details are given in the Supplemental Data.

### Supplemental Data

Supplemental Data for this article include Supplemental Experimental Procedures, two tables, and one figure and can be found with this article online at [http://www.current-biology.com/supplemental/S0960-9822\(09\)00630-7](http://www.current-biology.com/supplemental/S0960-9822(09)00630-7).

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